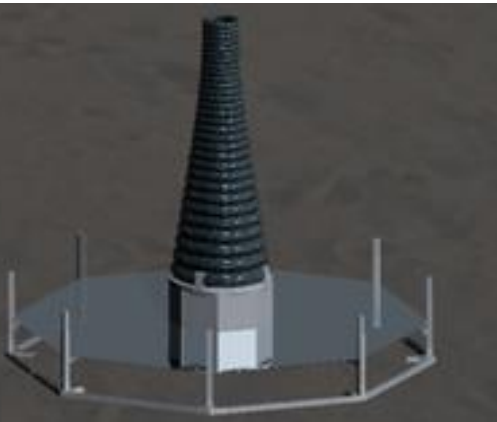


Applied Mathematical Evaluation of Solar Tower Systems: Hybrid Renewable Energy Development



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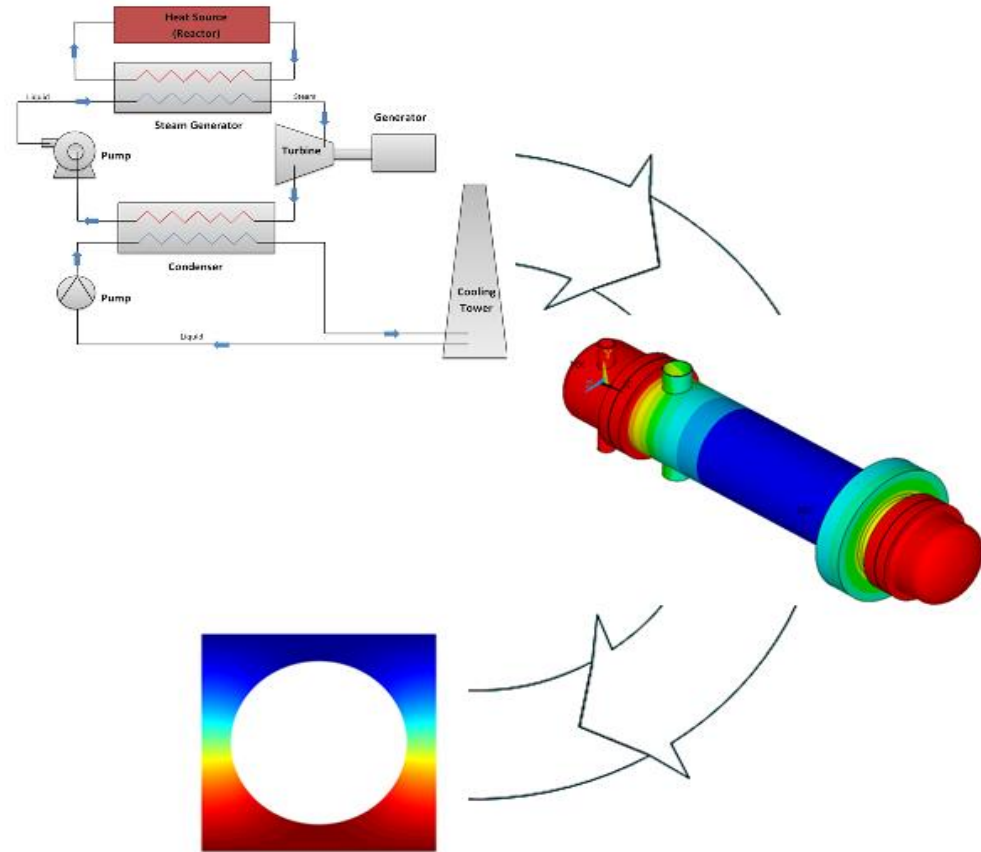
PIMS Workshop on Mathematical Sciences and Clean Energy Applications

ESB 1012, UBC

May 23, 2019

Outline

- Motivation and Background
- Analytical Study
- Double-Inlet Collector
- Inflatable Tower
- Combined Solar Cycle
- Related Investigations

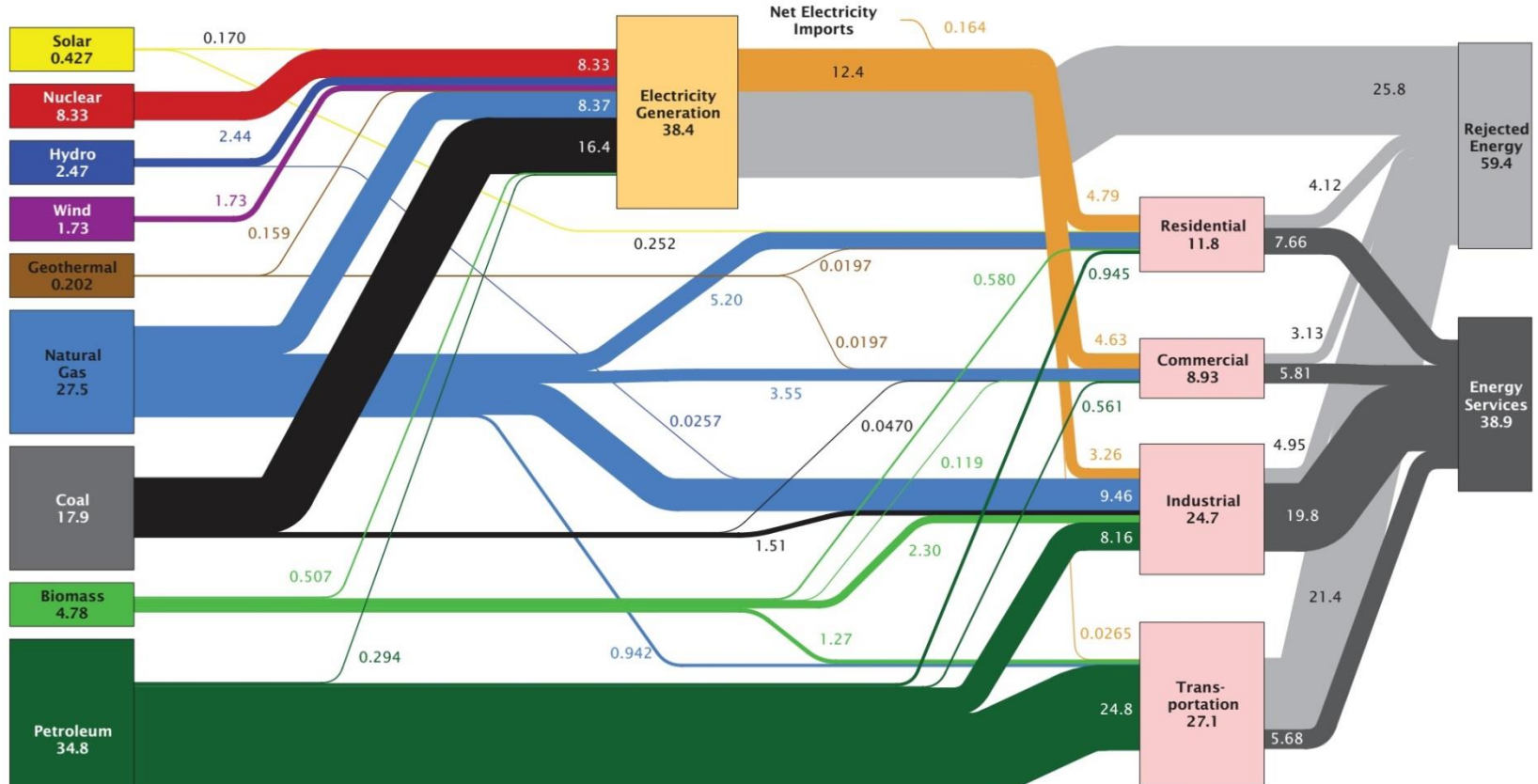


Motivation

- Fossil fuels are still the dominant source of energy.
- The share of solar energy is still very low (0.43% of the US energy consumption in 2015 and 0.58% in 2016)

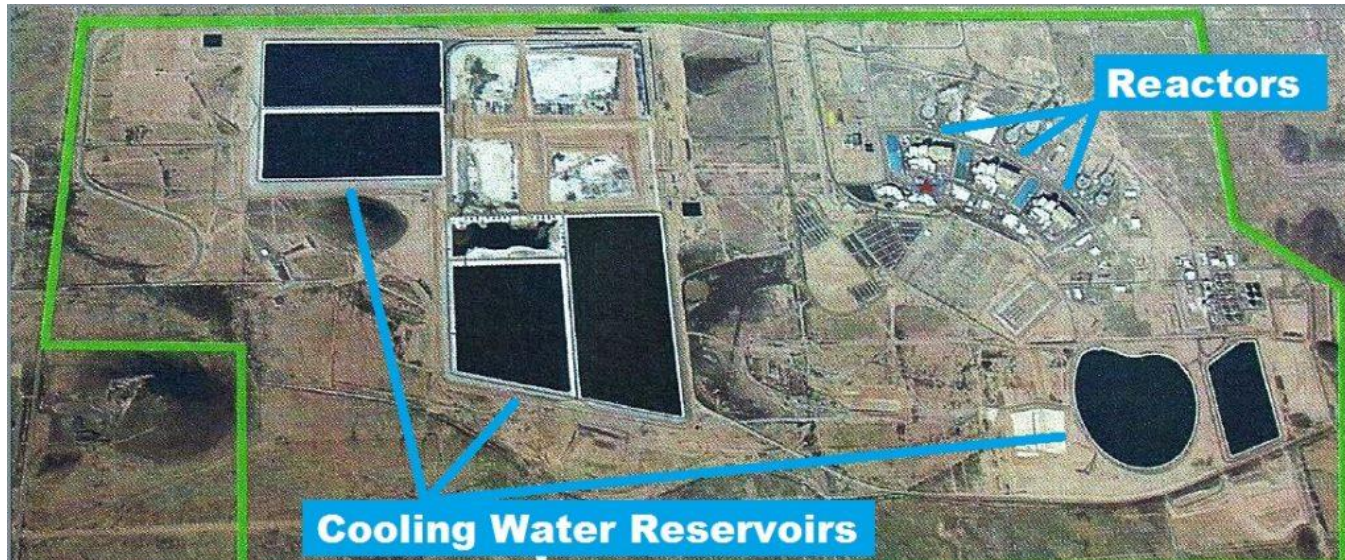
Motivation/Bad News!

units in quadrillion Btu



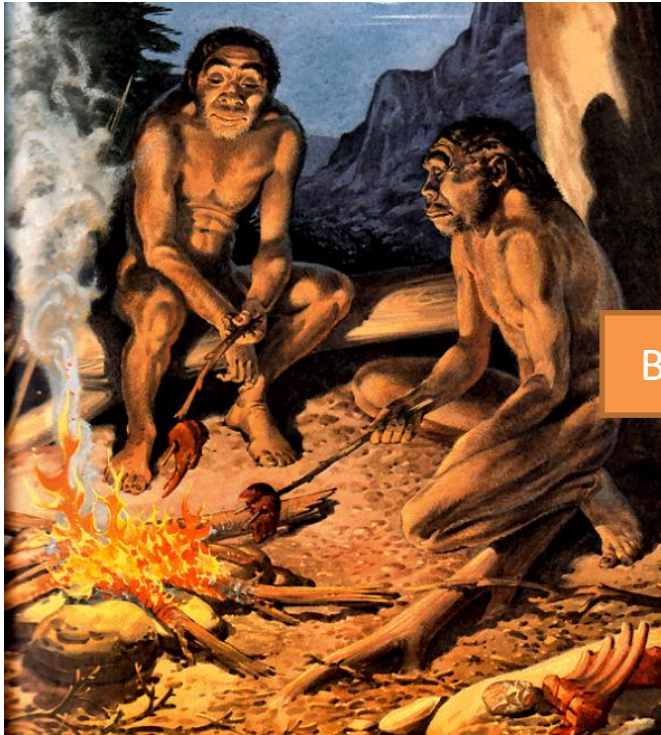
Nuclear energy provided around **8%** of the total primary energy consumption and all of it was used for electricity generation. The share of **solar energy** in 2015 US electricity generation was just **0.4%** in 2015 and **0.6%** in 2016.

Another Motivation/Bad News!



- The single **largest** consumers of fresh water in the United States are **thermal power plants** used to produce electricity.
- Approximately **half** of all fresh water consumed in the United States is used to absorb waste heat from thermal power plants.
- Typically, this water is either returned to the body of water from which it was extracted, or more commonly it is evaporated to the atmosphere in **a cooling tower**.
- Some nuclear power plants (Palo Verde in particular) are currently restricted from expansion by the lack of fresh water.

Similar Historical Approach



Burning wood or gas

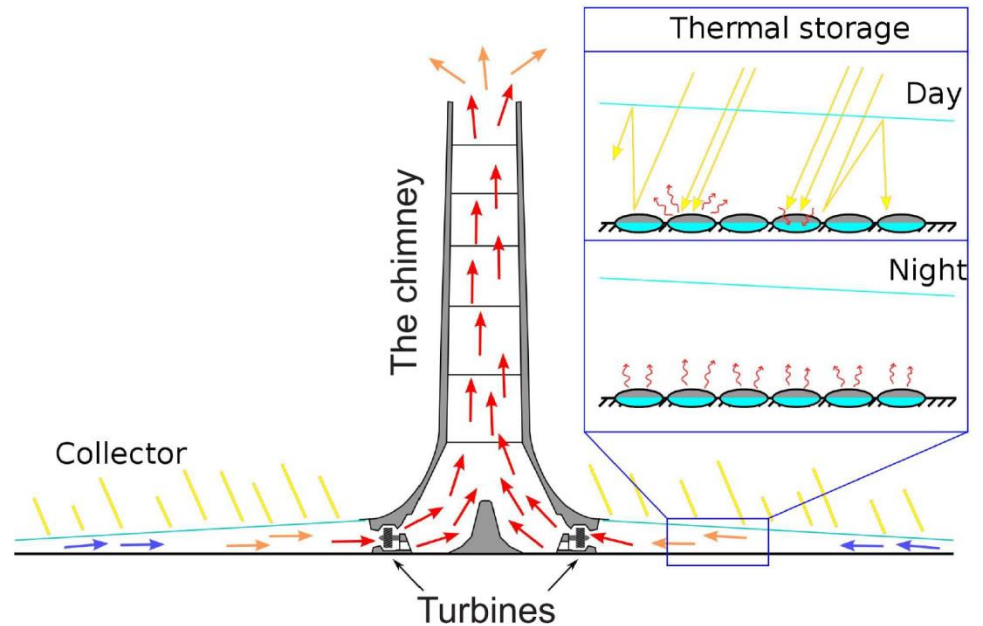


**No Change In Energy Policy for 300,000 Years,
Throw a Little Carbon on the Fire**

Solar Power Towers

- Concentrated Solar Power Plants
- Solar Chimney Power Plants

Solar Chimney Power Plant



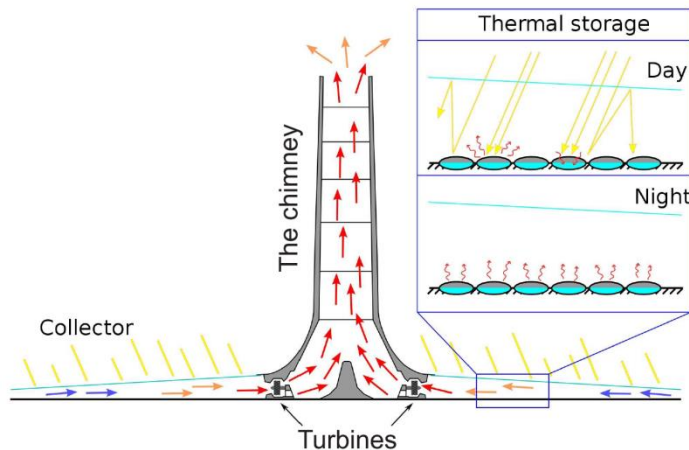
Our Goal

- Having solar towers more efficient to be utilized in hybrid energy systems
- To address the water consumption issue in the cooling process

Manzanares Prototype



Prototype component	Size (m)
Mean collector radius	122.00
Collector height	1.85
Chimney radius	5.08
Chimney height	196
Rotor blade length	5



- Isidoro Cabanyes, Spanish colonel proposed this idea(1903).
- The most famous prototype built in Manzanares at Spain in 1982 and rebuilt in 1989.
- China recently started to invest on this industry.

Analytical Study

$$\frac{dA}{A} + \frac{d\rho}{\rho} + \frac{du}{u} = 0 \quad (\text{Continuity})$$

$$dp + \rho u du = 0 \quad (\text{Momentum})$$

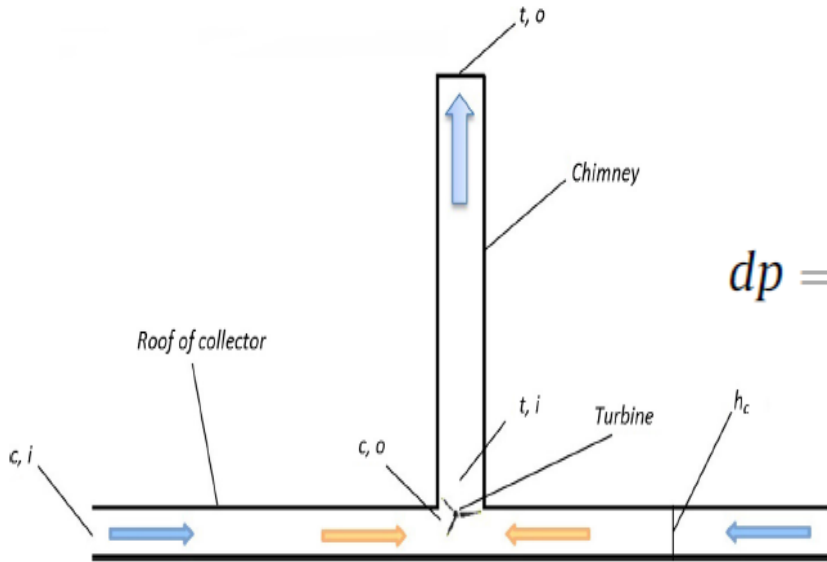
$$c_p dT - dq + u du = 0 \quad (\text{Energy})$$

$$dp = d(\rho RT) \quad (\text{State})$$

$$\dot{W} \simeq \frac{\dot{m}(p_{c,o} - p_{t,i})}{\rho_{turb}}$$



Analytical Study-Collector



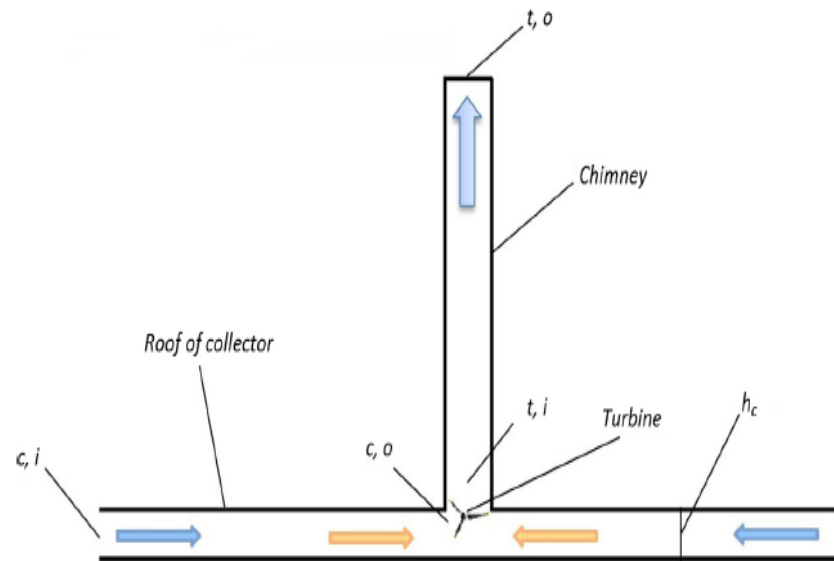
$$dp = \frac{\dot{m}^2}{\rho} \left(\frac{dA}{A^3} - \frac{q''(2\pi r)dr}{\dot{m}(2\pi r h_c)^2 T c_p} + \frac{u du}{A^2 c_p T} + \frac{dp}{A^2 p} \right)$$

$$p_{c,o} - p_{c,i} \simeq \left[\frac{\dot{m}^2}{2\rho_{m,c}} \left(\frac{1}{A_{c,i}^2} - \frac{1}{A_{c,o}^2} \right) + \frac{q''\dot{m}}{2\pi h_c^2 c_p \rho_{m,c} T_{m,c}} \ln \frac{r_{c,i}}{r_{c,o}} \right]$$

Analytical Study-Tower

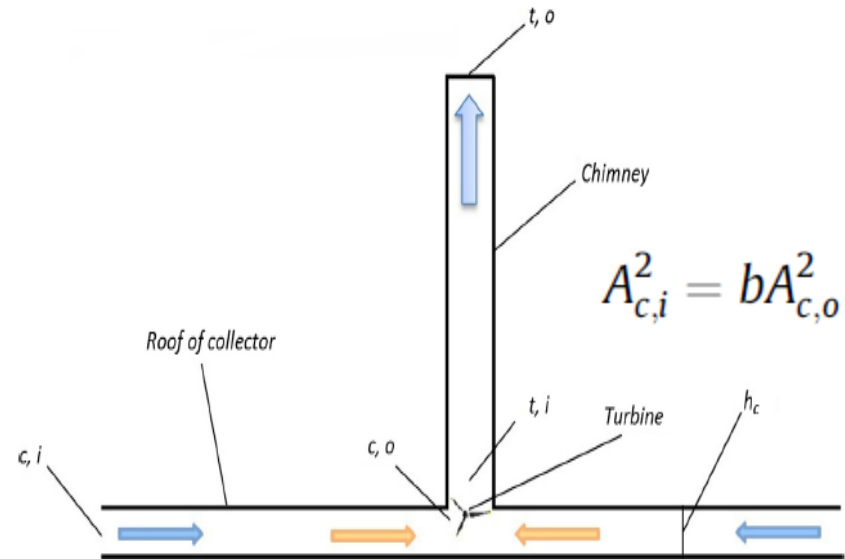
$$p_{t,o} = p_{\infty} \left(1 - \frac{gh_t}{c_p T_{\infty}} \right)^{\left(\frac{c_p}{R} \right)}$$

$$\rho_{t,i} = \rho_{c,o} = \rho_{\infty} \left(1 + \frac{T_{\infty} - T_{c,o}}{T_{\infty}} \right)$$



$$p_{t,o} - p_{t,i} \simeq -\rho_{m,t} gh_t - \frac{\dot{m}^2}{2\rho_{m,t}} \left(\frac{1}{A_{t,o}^2} - \frac{1}{A_{t,i}^2} \right)$$

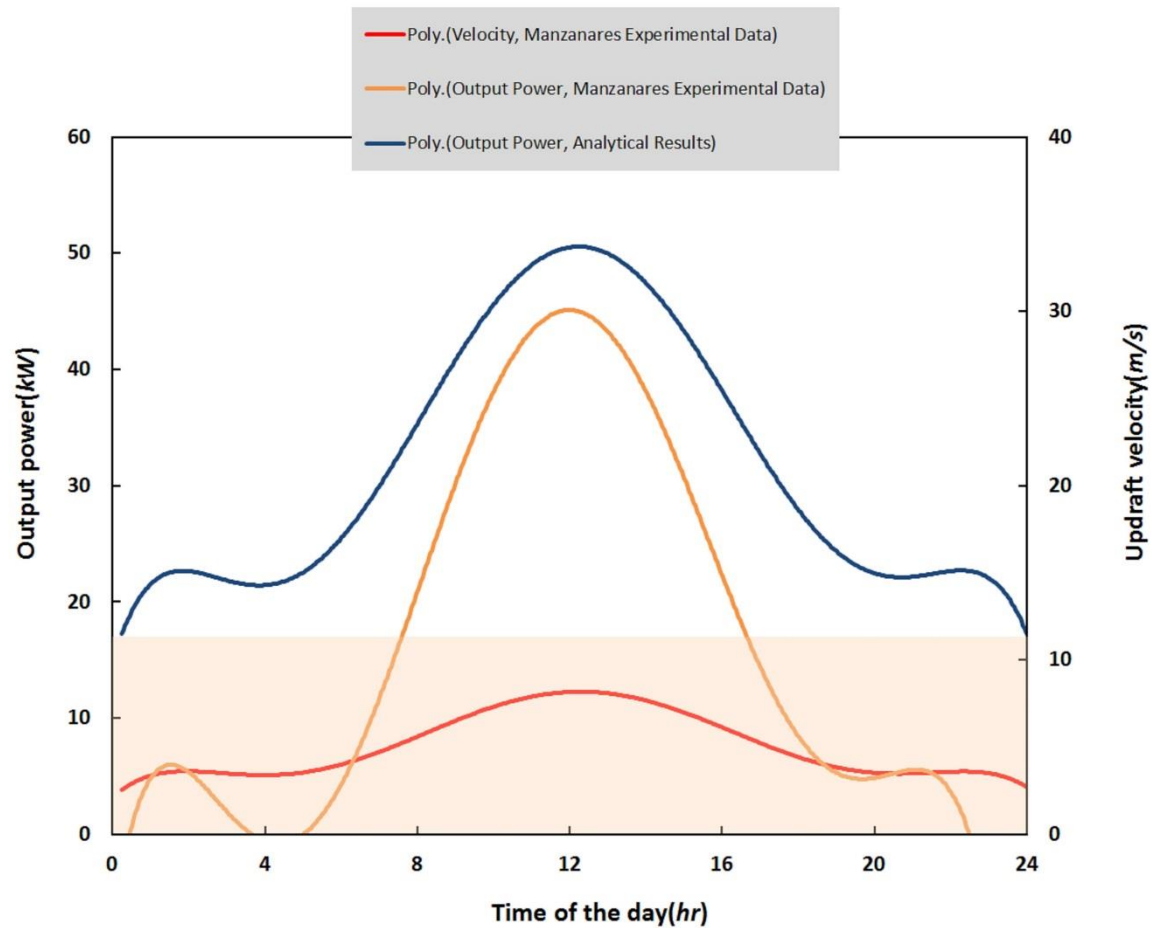
Analytical Study-Power Calc



$$\dot{W} \simeq \frac{\dot{m}(p_{c,o} - p_{t,i})}{\rho_{turb}}$$

$$\dot{W} \simeq \frac{\dot{m}}{(\rho_{c,o} + \rho_{t,i})/2} \left[\frac{-\dot{m}^2}{2\rho_{m,c}} \left(\frac{b-1}{bA_{c,o}^2} \right) + \frac{q''\dot{m}}{2\pi h_c^2 c_p \rho_{m,c} T_{m,c}} \ln \frac{r_{c,i}}{r_{c,o}} + (\rho_\infty - \rho_{m,t})gh_t \right]$$

Analytical Study-Power Calc.

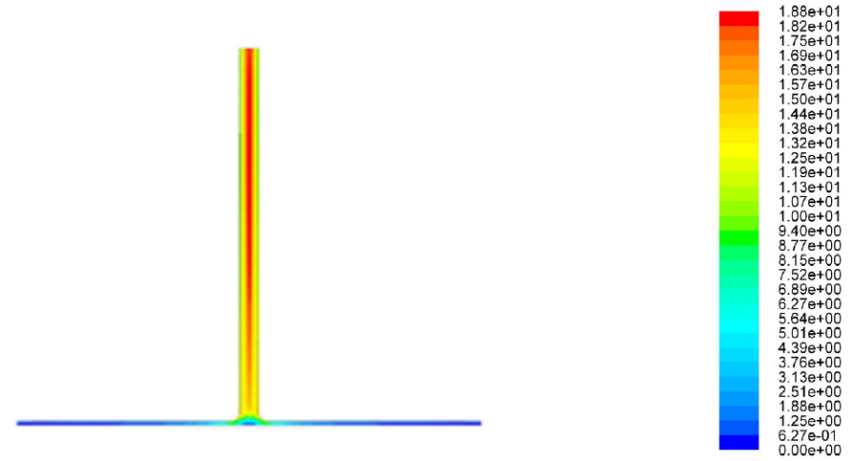
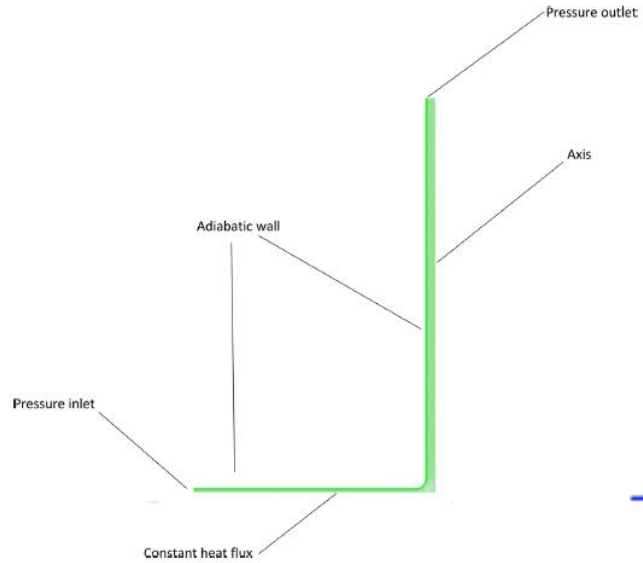


Computational Study

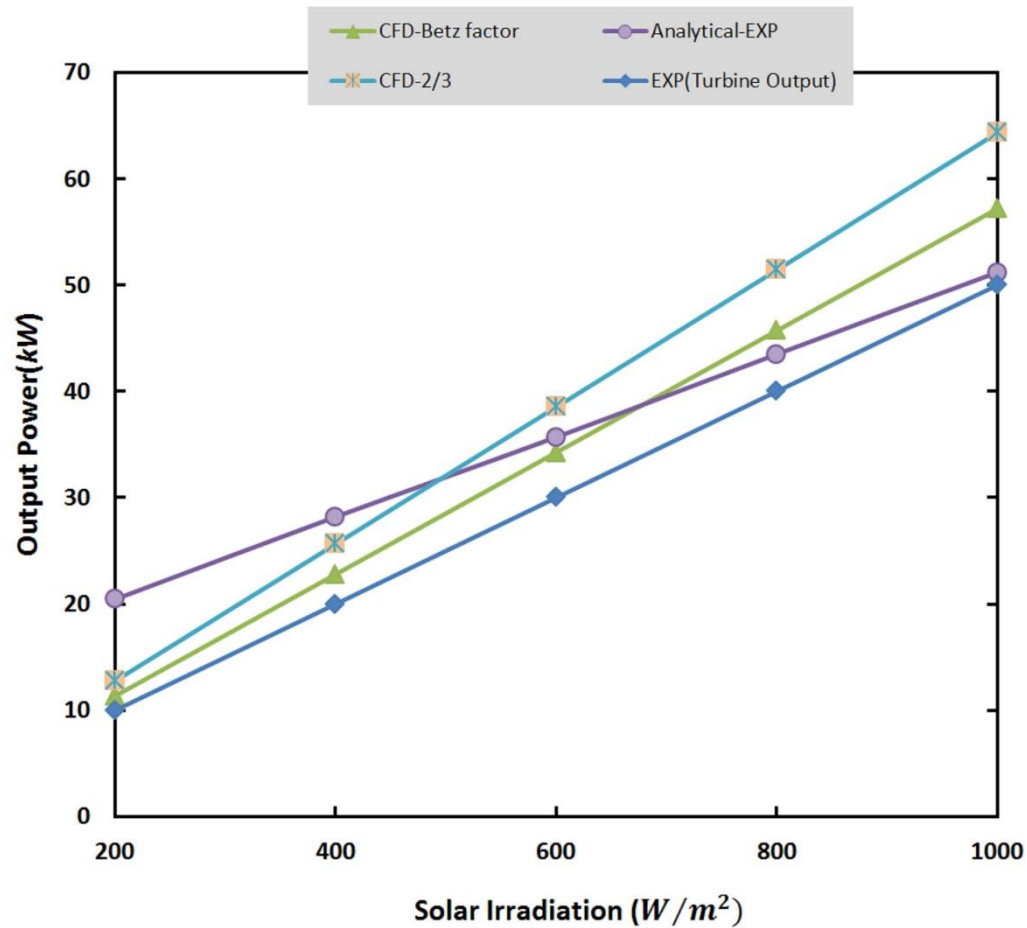
Turbulent
Flow

Air

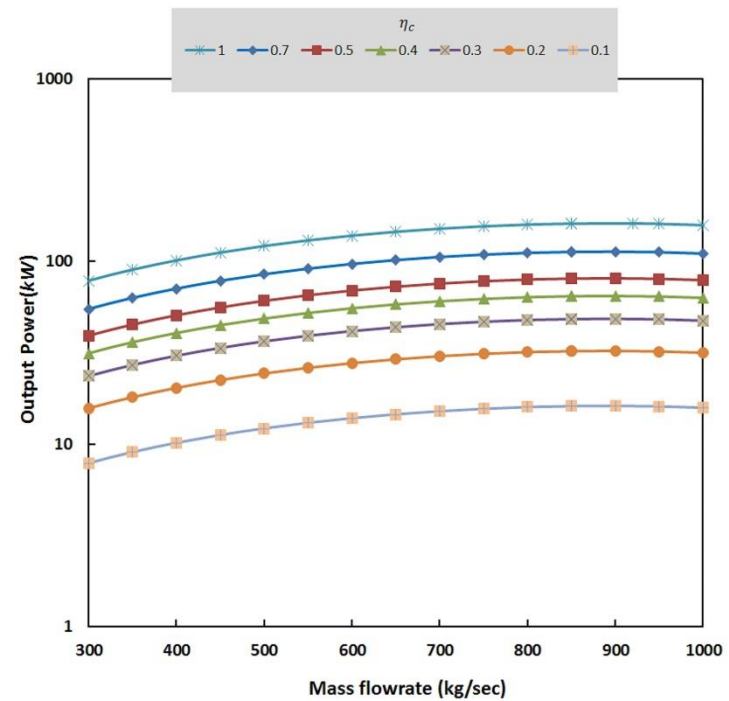
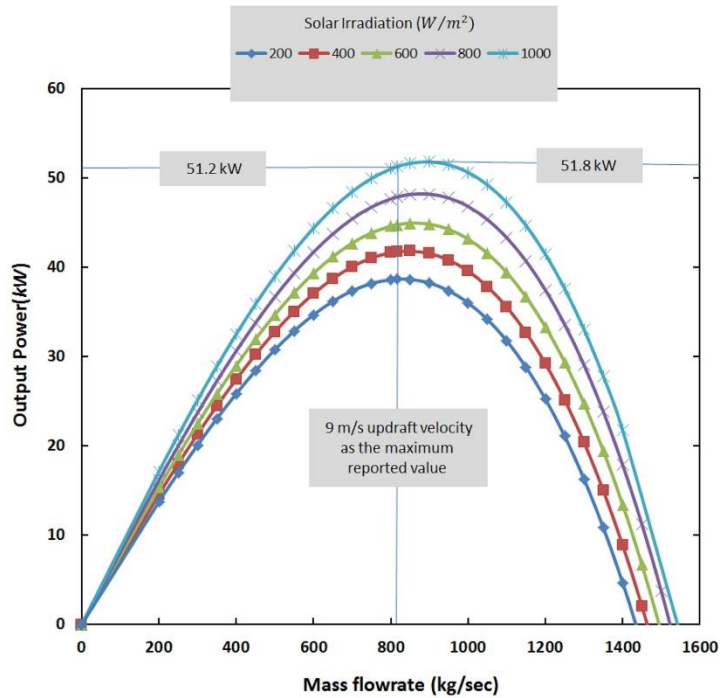
Natural
Convection



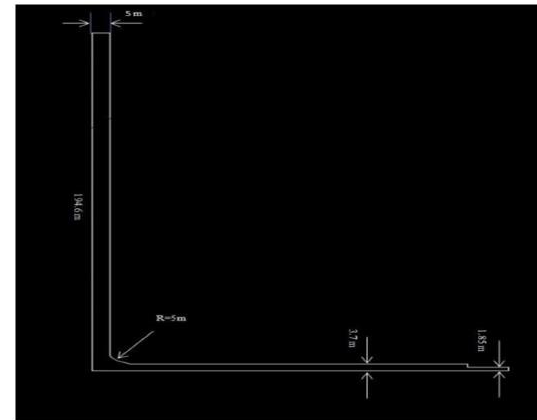
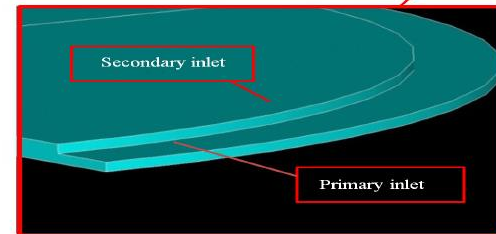
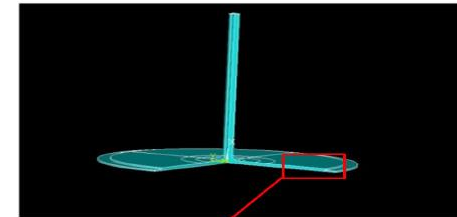
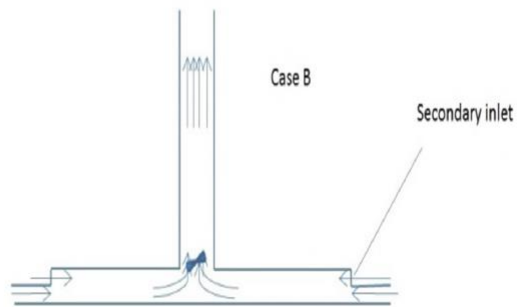
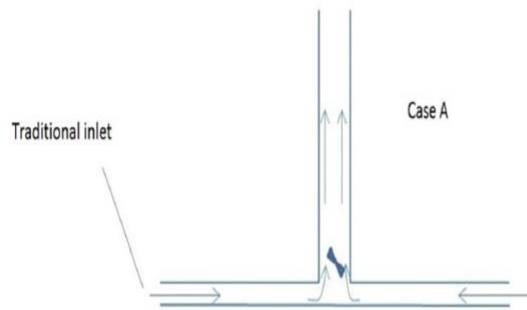
Comparative Study - Evaluation



Analytical Power



Double-Inlet Collector



Analytical Approach

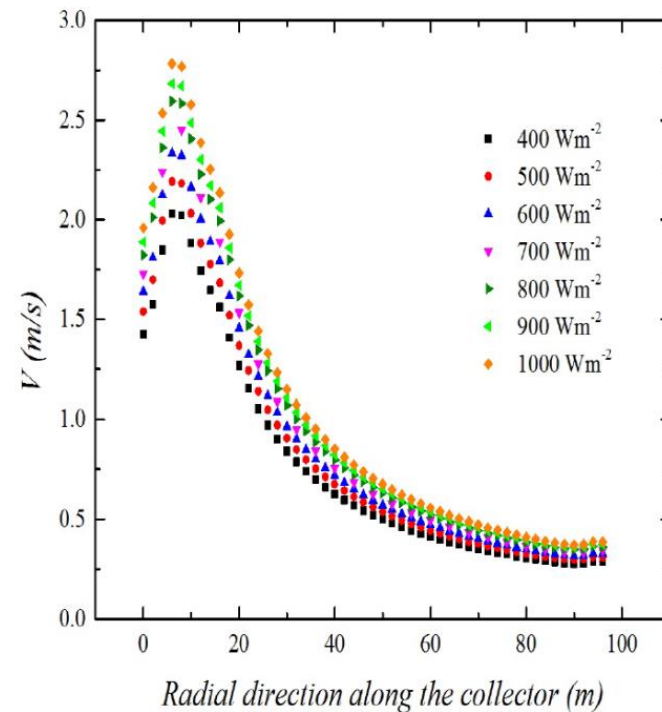
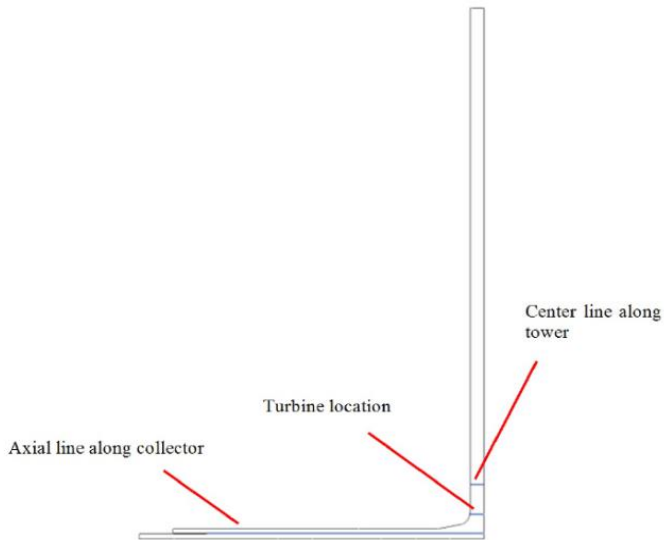
$$\dot{m}_{i_2} = 2\pi r(h_{c,i_2} - h_{c,i_1})u_{i_2}$$

$$u_{i_2} = u_{ref} \left(\frac{h_{c,i_2}}{h_{ref}} \right)^\alpha$$

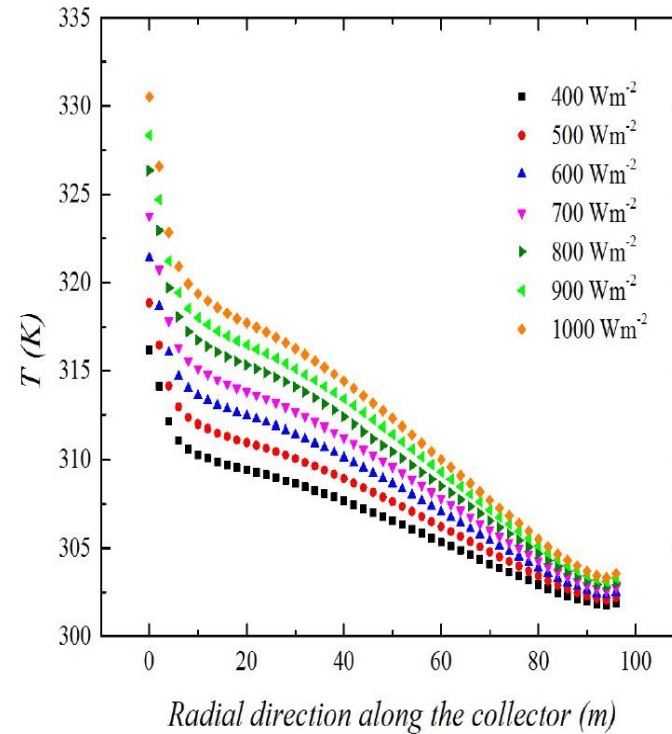
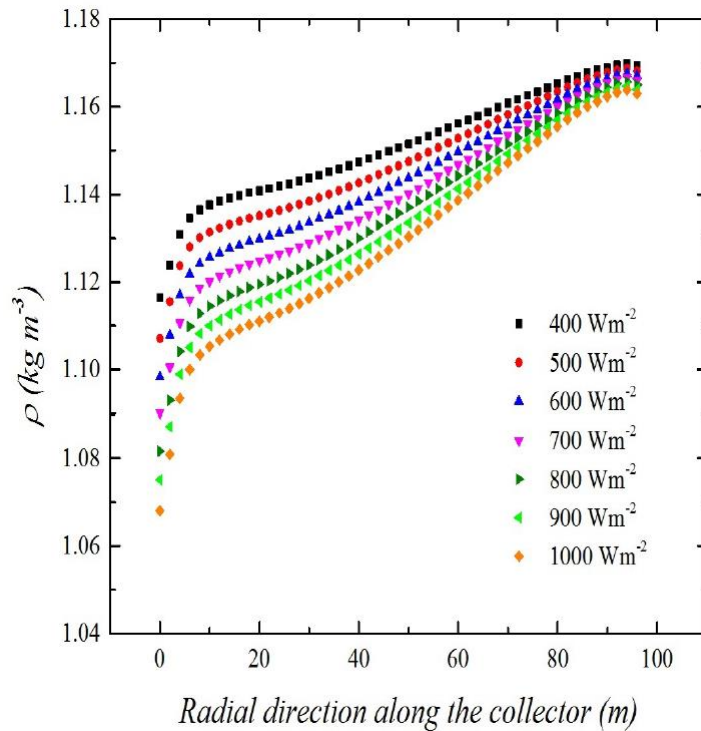
$$\alpha = 1/\ln(h_{ref}/h)$$

u_{ref} is the wind velocity measured at h_{ref} which is considered as the reference wind velocity value, and α is the wind shear exponent.

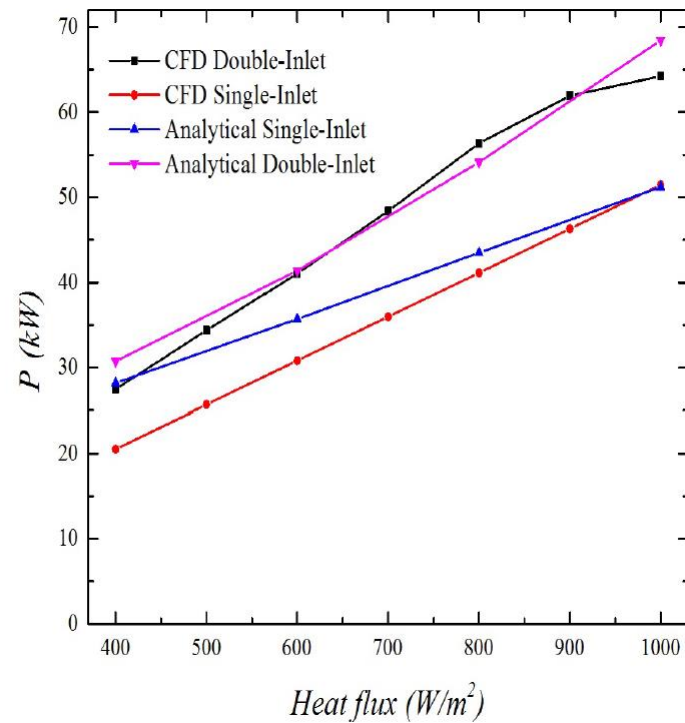
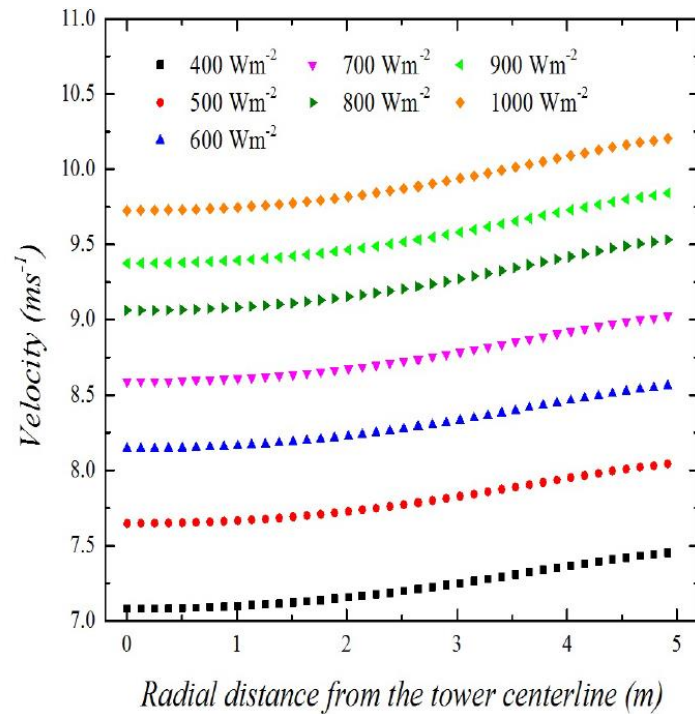
Double-Inlet Collector Numerical Analysis



Numerical Analysis

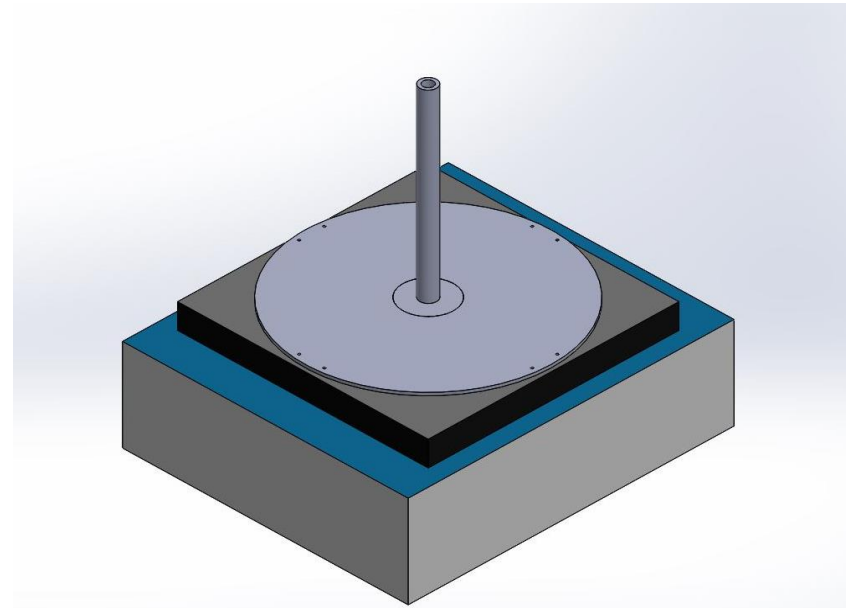


Numerical Analysis

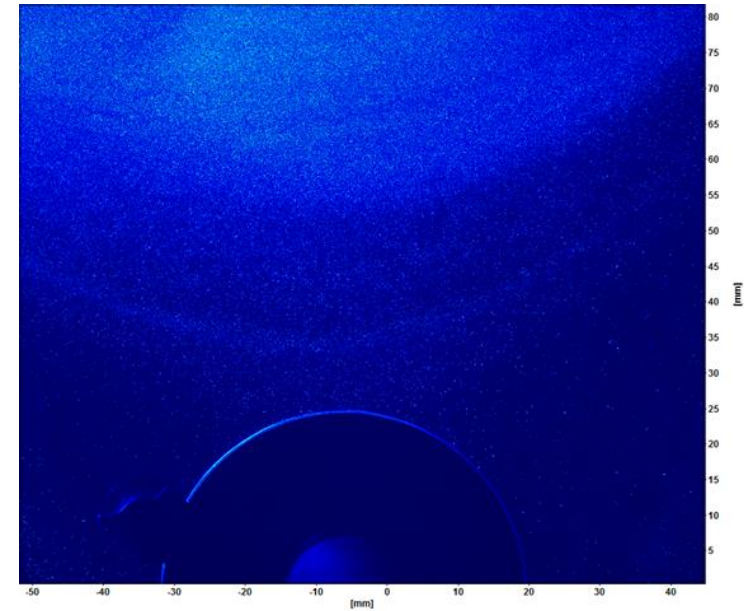
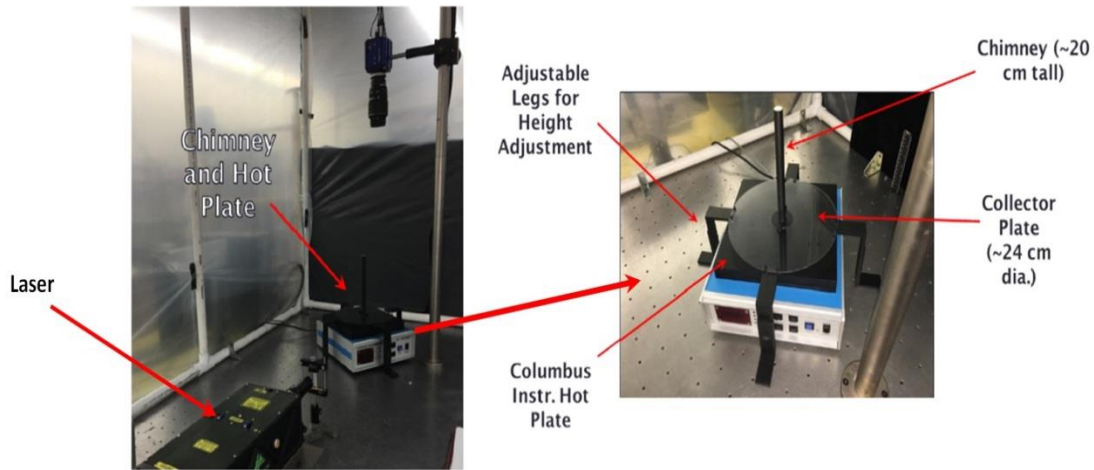


Experiments

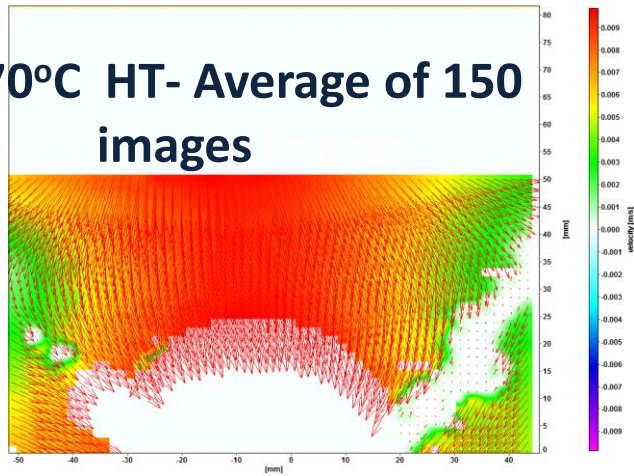
“A computer lets you make more mistakes faster than any invention in human history— with the possible exceptions of handguns and tequila.”- Mitch Ratcliffe



Experimental Analysis



70°C HT- Average of 150 images

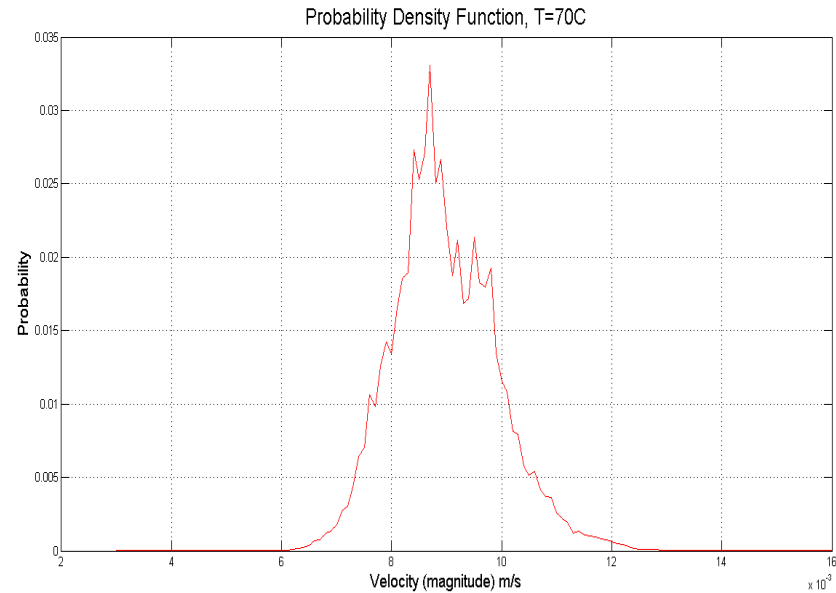


Experimental Results

- Mean:

$$u = 9.01 \text{ mm/s}$$

$$u \in [7.21, 10.7] \frac{\text{mm}}{\text{s}}$$



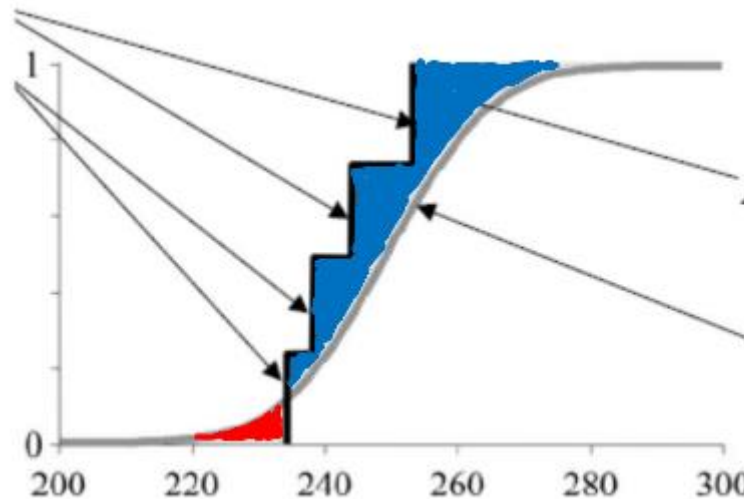
Examples of the Area Validation Metric

▶ The modified form for CDF has a separate tracking

▶ Experiments **larger** than simulation, d^+

▶ Experiments **smaller** than simulation, d^-

$[S + F_s d^-, S + F_s d^+]$ where $F_s = 1.25$

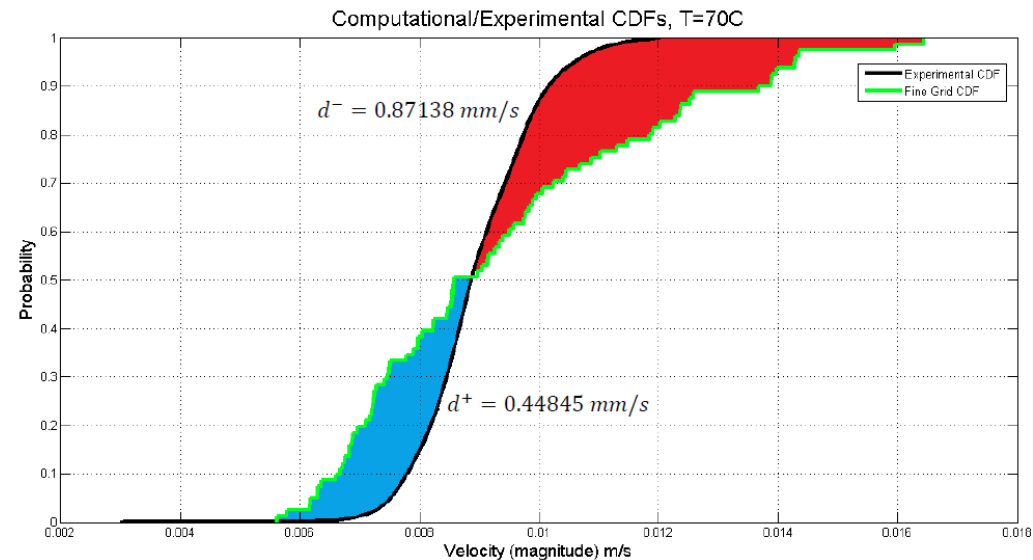


Mismatch Representation

We can represent the model form uncertainty in an interval by having the mismatch.

- $$u_{model} = [S - F_s d^-, S - F_s d^+] \frac{mm}{s} = [8.15, 10.3] \frac{mm}{s}$$
- S is the simulation results
- d represents the mismatch

The **validation metric** is defined to be the area between the EDF/CDF from the simulation and the EDF/CDF from the experiment.



Model Verification

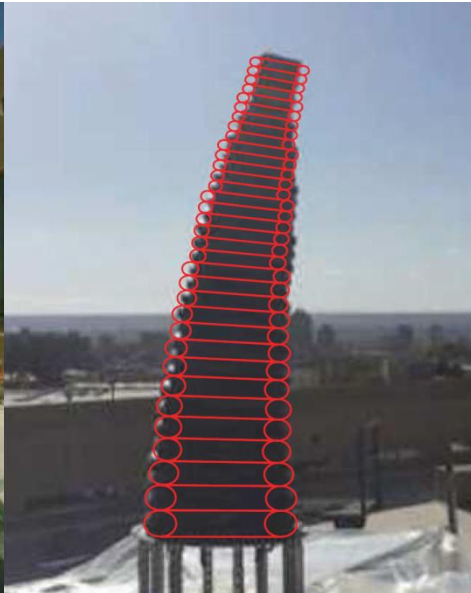
- Observed order of accuracy: $\hat{p} = 1.043$

$$\hat{p} = \frac{\ln\left(\frac{f_3 - f_2}{f_2 - f_1}\right)}{\ln(r)} \quad r = \frac{h_2}{h_1} = \frac{h_3}{h_2}$$

- Estimated exact solution (RE): $\bar{u} = 10.508$ mm/s
- Estimated DE: $\varepsilon_h = 0.1154$ mm/s
- Grid Convergence Index: $GCI = 0.3463$ mm/s

$$\varepsilon_h \cong u_h - \bar{u}$$

Inflatable Tower



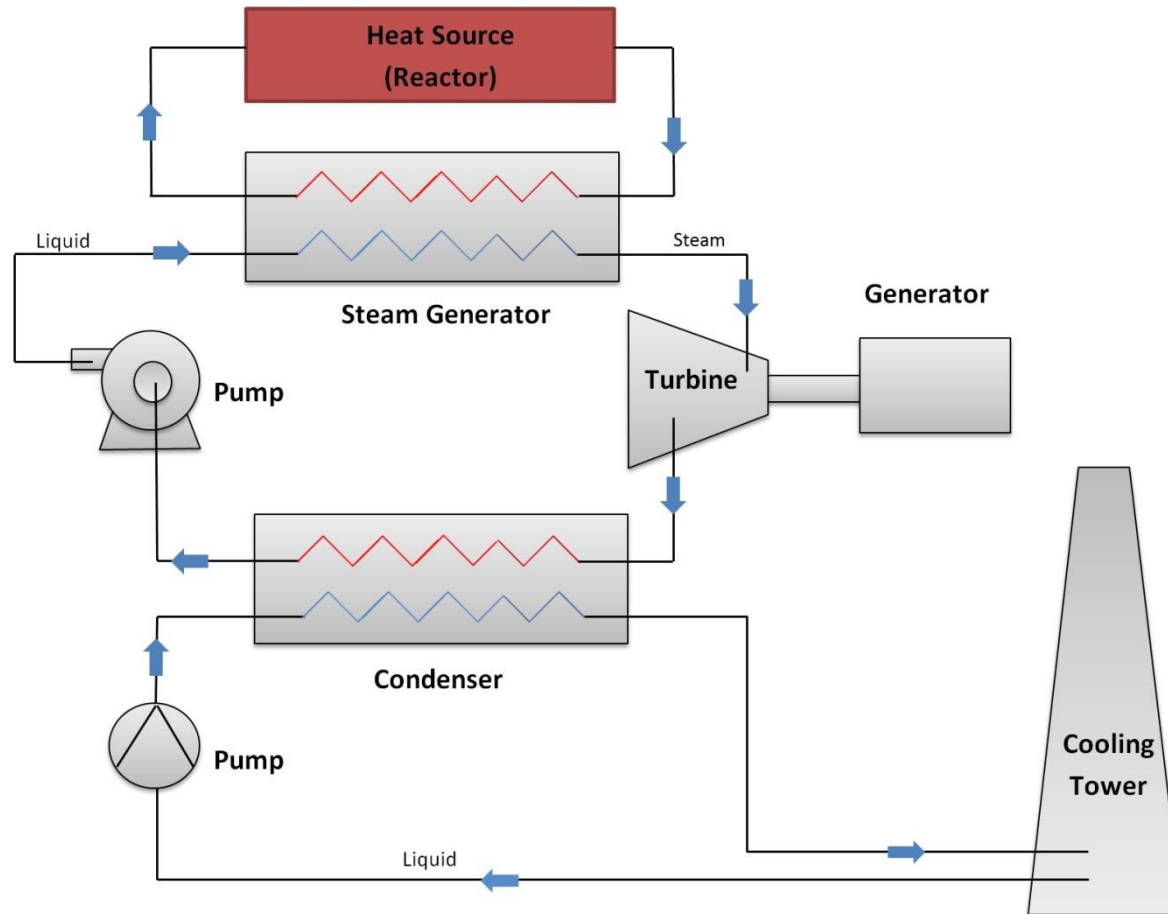
2 m/s



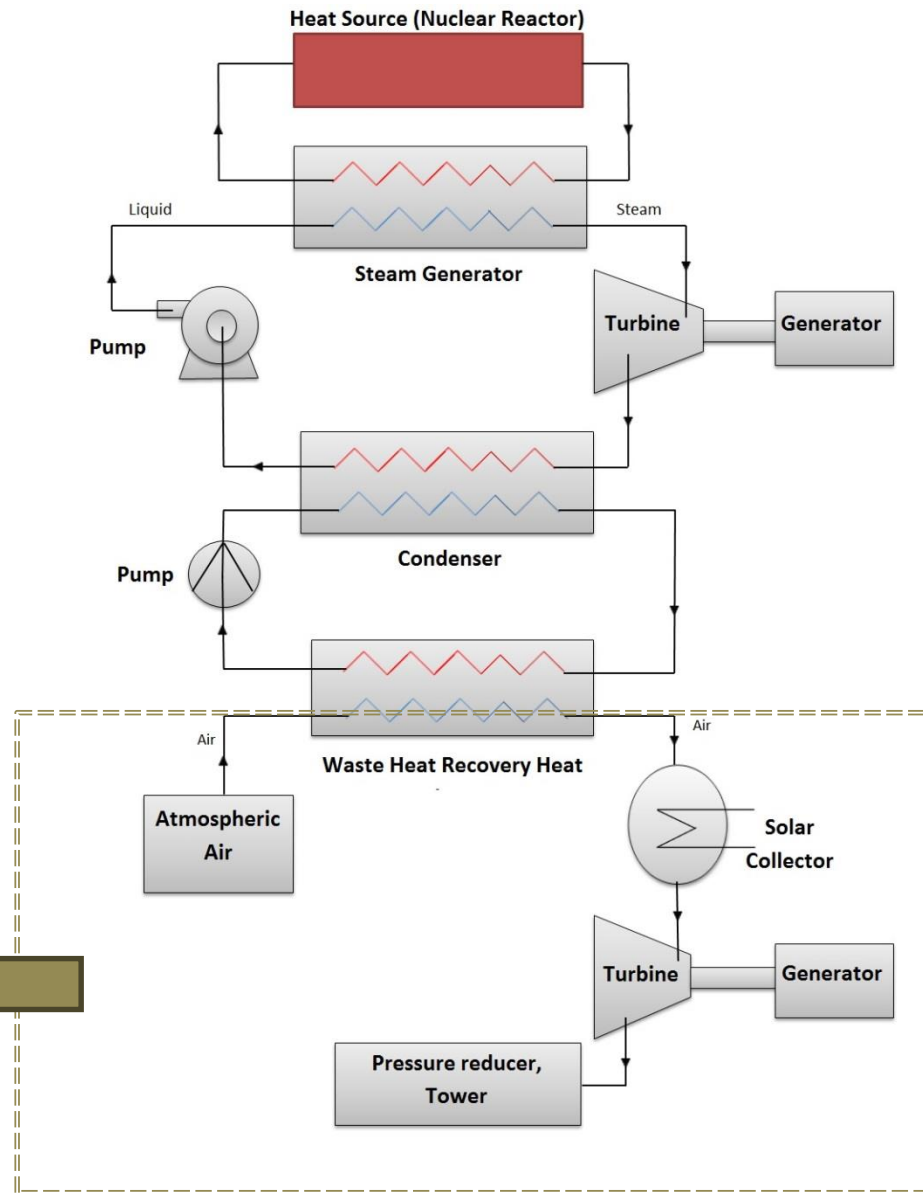
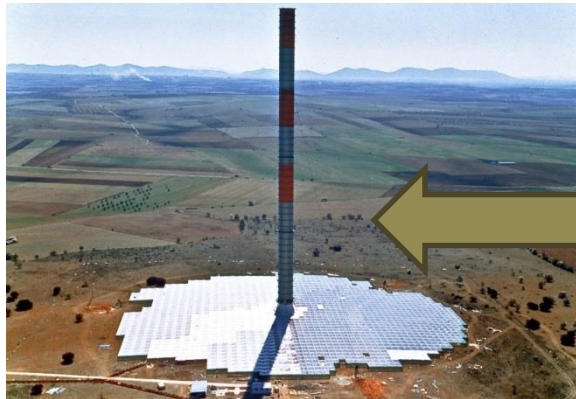
15 m/s

Combined Cycle

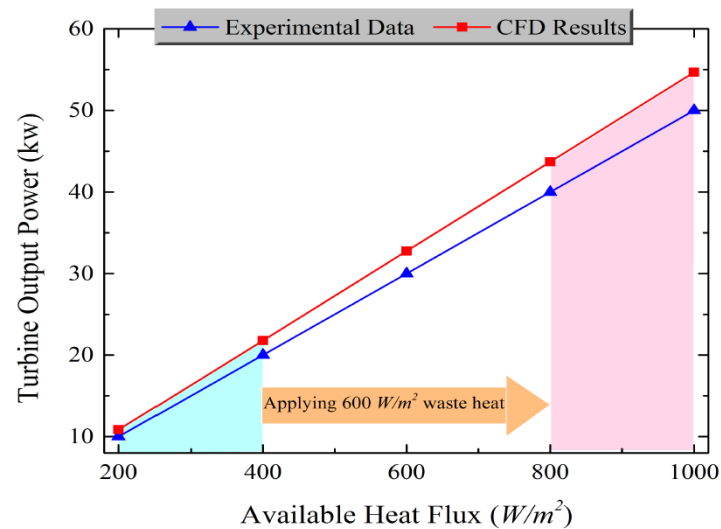
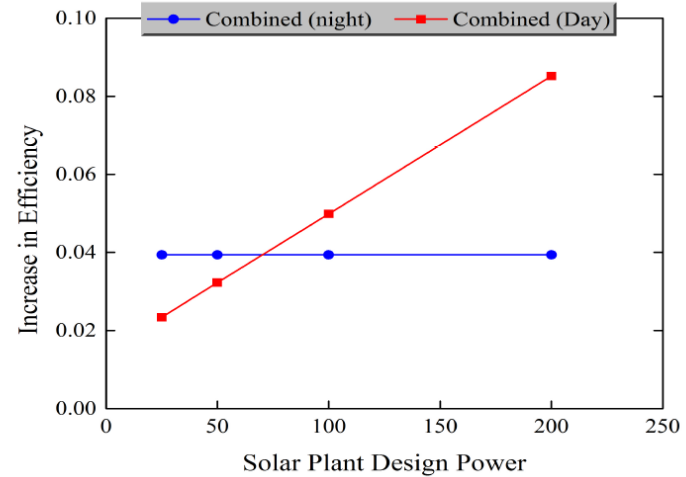
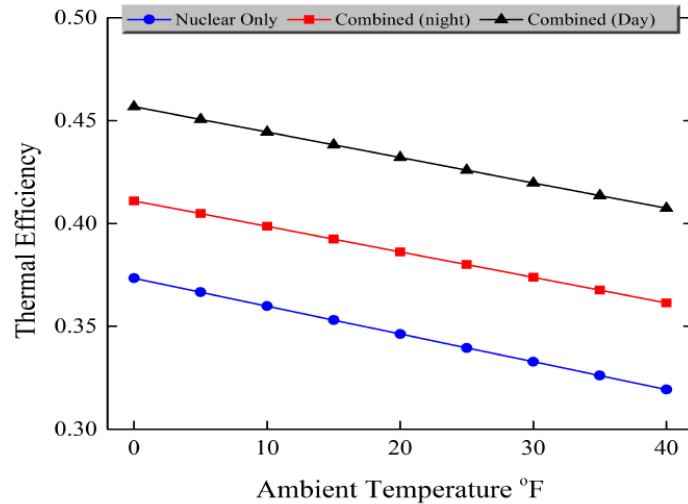
Thermal Cycle of a PWR



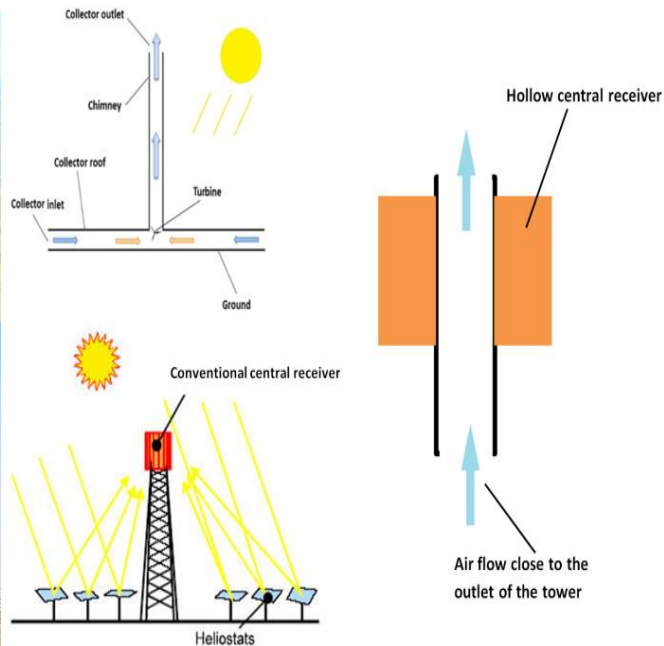
The Proposed Cycle



Combined Solar Cycle



On going work



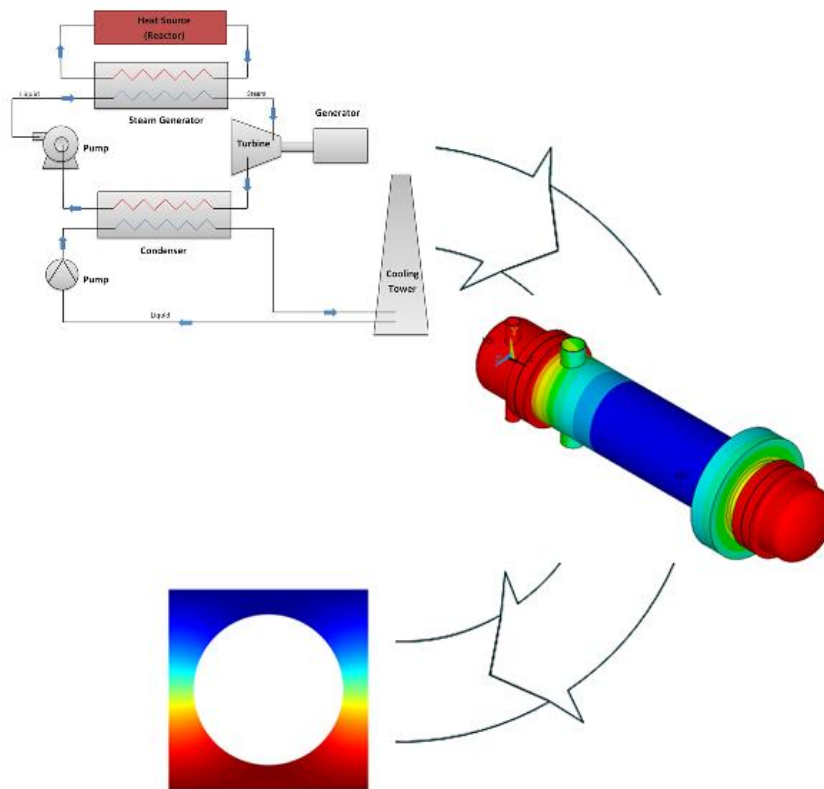
**Optimal collector shape:
roof and ground***

Heat waste recovery**

*Will be presented at the next ☺ PIMS Workshop on Mathematical Sciences and Clean Energy Applications

** Sponsored by Compo Energy

Heat Exchanger



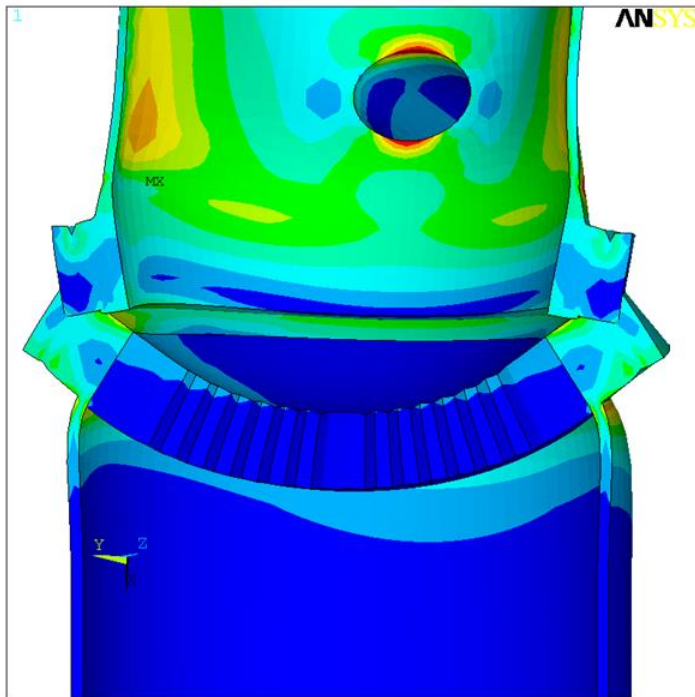
Heat exchanger is a key component in any thermal power cycle. Thermal design and numerical model especially for high temperature and pressure applications

Computational and experimental inspection and testing per ASME codes

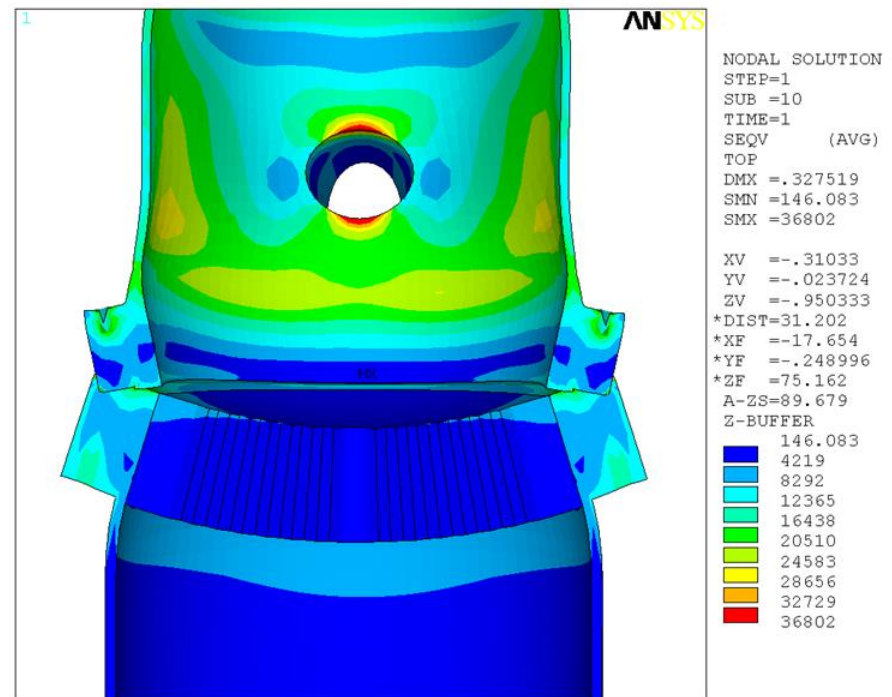
Propose enhancement in thermal-hydraulics performance of HX

Involving advanced manufacturing to fabricate

Excessive distortion of tubesheet due to temperature differential



Initial design
 (T.S. 4 7/8") (150X magnification)

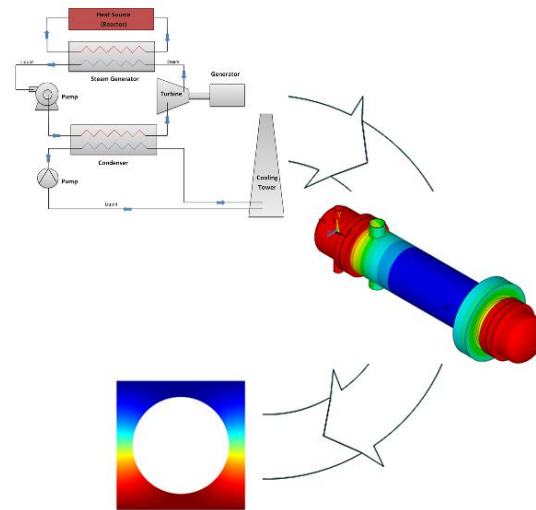


Final Design
 (T.S. 8") (150X magnification)

Thermal Response

Important aspect in HX for inspection and testing

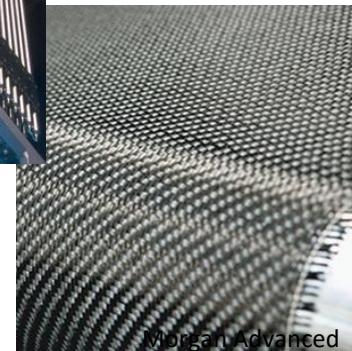
- Cladding
- Thermal fatigue
- Porous composite



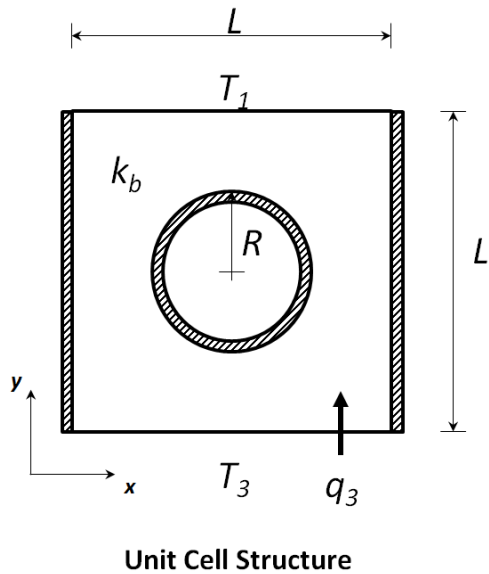
Effective thermal material properties of the applied composite shall be evaluated

More Applications

- Porous media
 - Materials & structures containing voids of different phases
- Examples
 - Aerogels
 - 3D-printed structures
 - Nuclear fuel assemblies
 - Carbon composites
 - Pipelines



Computational Model

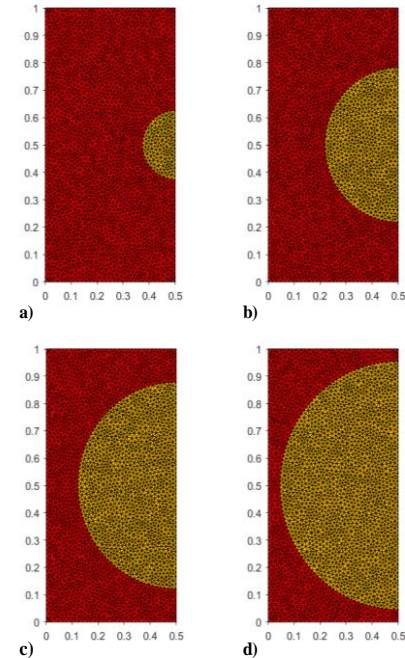
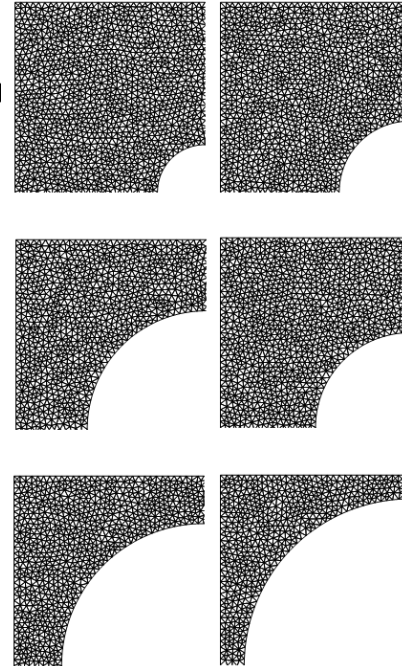


Unit Cell Structure

- k_b = bulk thermal conductivity
- k^* = dimensionless effective thermal conductivity
- L = cell length & width
- q = heat flux
- R = void radius
- T = temperature
- α = porosity

$$\alpha = \frac{\pi R^2}{L^2}$$

$$k^* = \frac{q_3 L}{k_b (T_3 - T_1)}$$



Code Verification

Method of Manufactured Solutions (MMS)

Solution

$$T_{MMS}(x,y) = \cos(x\pi/L) \sin(y\pi/L + 0.75)$$

Source Term

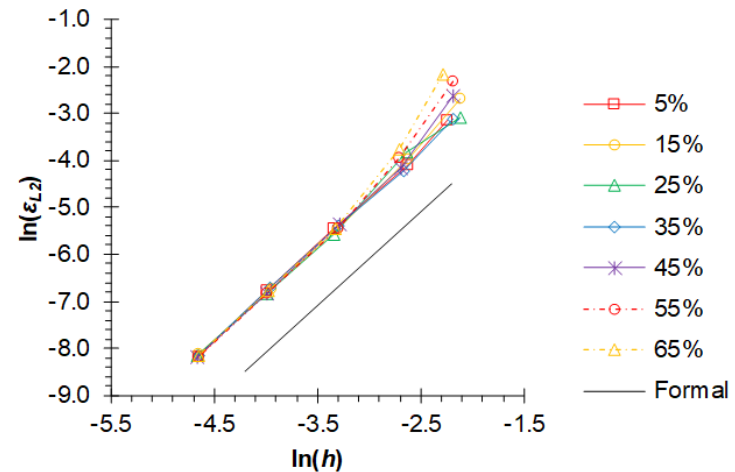
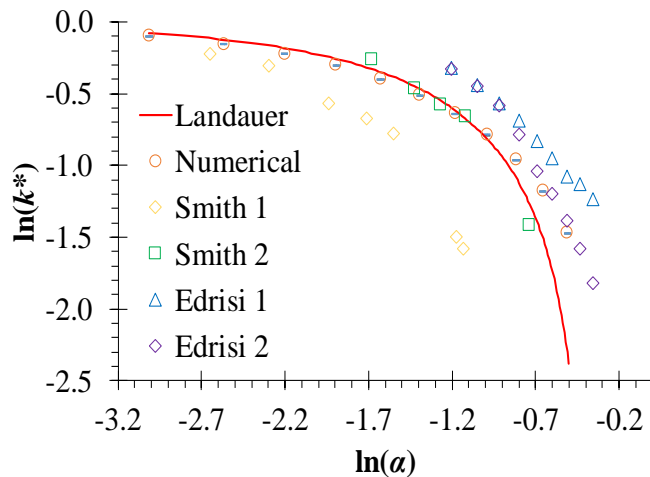
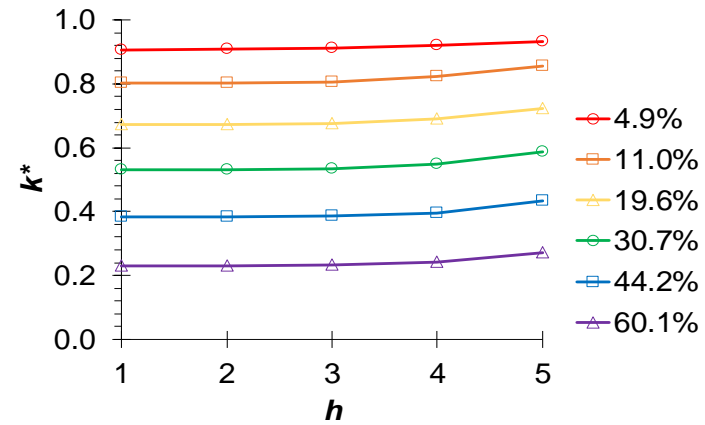
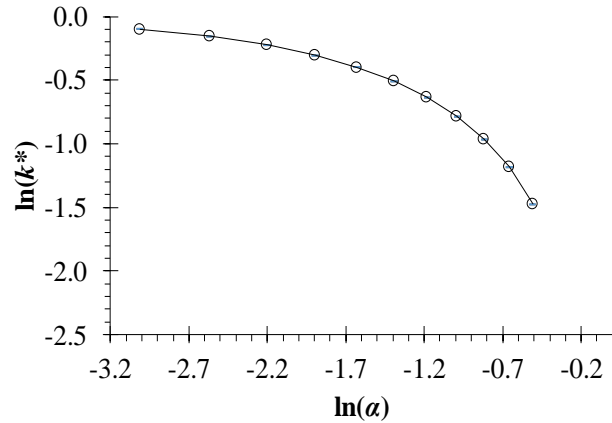
$$Q_{MMS}(x,y) = (k_x) \cos\left(\frac{x\pi}{L}\right) \sin\left(\frac{y\pi}{L} + 0.75\right) \frac{\pi^2}{L^2}$$

Error

$$\epsilon_h = \sqrt{\sum_{i=1}^{N_V} [T_i - T_{MMS}(x_i, y_i)]^2 / N_V}$$

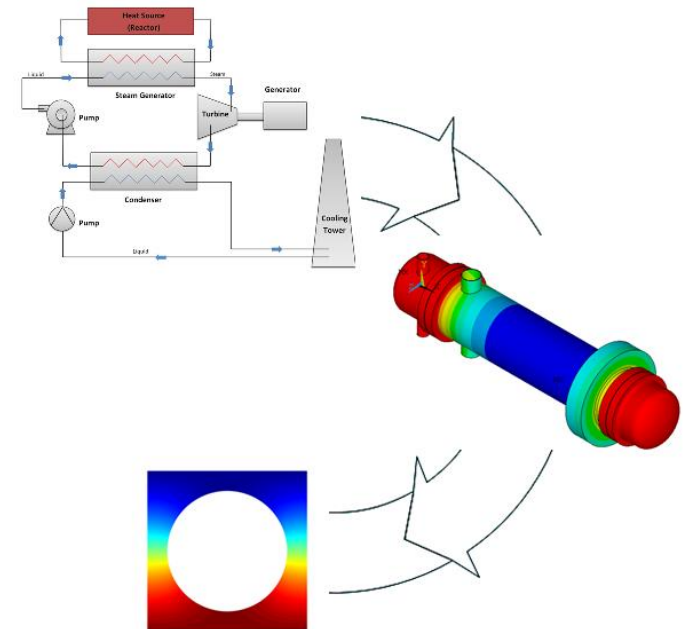
α	k^*	k^*_{ext}	p	ϵ_a	ϵ_{ext}	GCI	$U_{num,1}$	$U_{num,2}$
%	---	---	---	%	%	%	---	---
4.9	0.91	0.91	1.55	0.14	0.08	0.10	0.0009	0.0019
7.7	0.86	0.86	1.92	0.15	0.05	0.07	0.0006	0.0007
11.0	0.80	0.80	1.68	0.15	0.07	0.09	0.0007	0.0014
15.0	0.74	0.74	1.82	0.15	0.06	0.07	0.0005	0.0009
19.6	0.67	0.67	2.09	0.15	0.05	0.06	0.0004	0.0006
24.9	0.60	0.60	1.98	0.15	0.05	0.07	0.0004	0.0004
30.7	0.53	0.53	2.14	0.16	0.05	0.06	0.0003	0.0007
37.1	0.46	0.46	1.94	0.18	0.06	0.08	0.0004	0.0004
44.2	0.38	0.38	2.06	0.20	0.06	0.08	0.0003	0.0004
51.8	0.31	0.31	2.22	0.23	0.07	0.08	0.0003	0.0007
60.1	0.23	0.23	1.90	0.30	0.11	0.14	0.0003	0.0005

Some Results



Summary

- **Hybrid clean energy systems can be a solution to provide a more stable baseline of energy**
- **Design, development and modeling advanced hybrid clean energy power cycle are presented**
- **Computational fluid dynamics and heat transfer evaluation of energy conversion components**
- **Experimental prototype analysis was performed to validate our numerical model**





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Thank you!
Questions?

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